

Cryogenic Light Detectors for the CRESST Experiment

Anja Tanzke

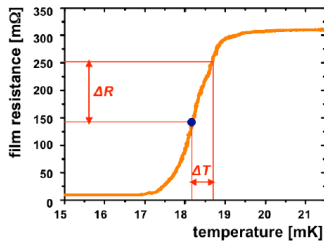
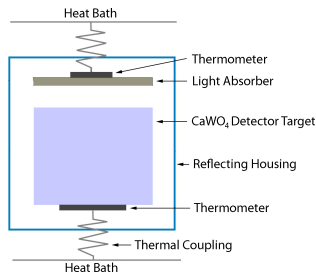
Max-Planck-Institute for Physics

IMPRS Workshop at Castle Ringberg
July 26th, 2012

CRESST Detector Module

- Measurement of phonon and light signal
 - Phonon Channel
 - Light Channel

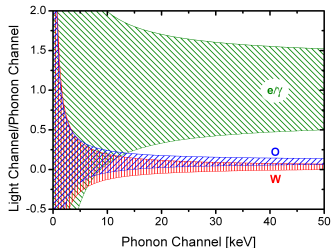
- Signals measured with Transition Edge Sensors (TES) as thermometers



Light-Phonon-Plane

Coincident light phonon measurement enables event identification

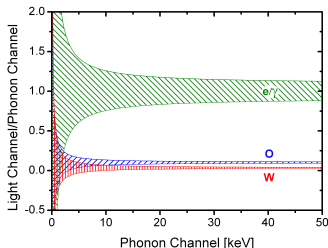
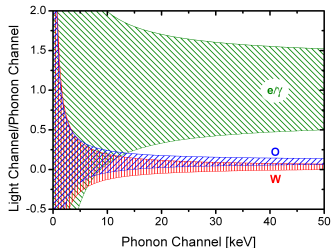
- Typical energy resolution of current detector module



Light-Phonon-Plane

Coincident light phonon measurement enables event identification

- Typical energy resolution of current detector module
- Light channel energy resolution improved by a factor of 5

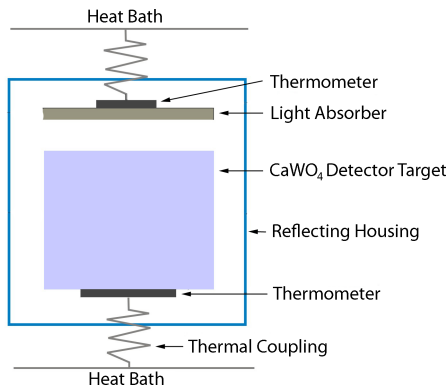


Width of the bands is determined by the light channel energy resolution

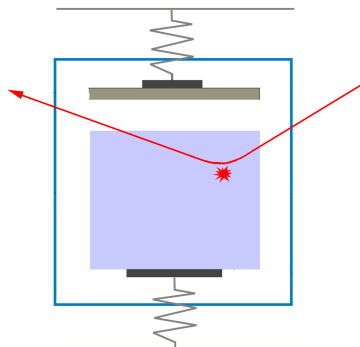
Goal

Improvement of the light channel's signal-to-noise ratio $\frac{E}{\Delta E}$

Energy Signal measured in the Light Channel

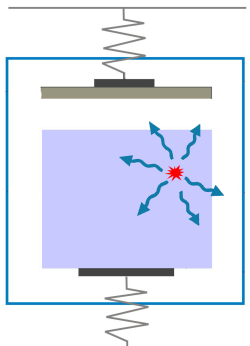


Energy Signal measured in the Light Channel



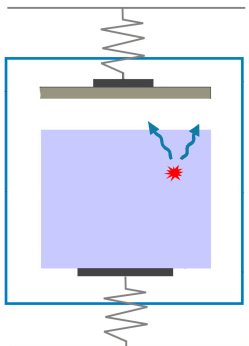
E_{dep}

Energy Signal measured in the Light Channel



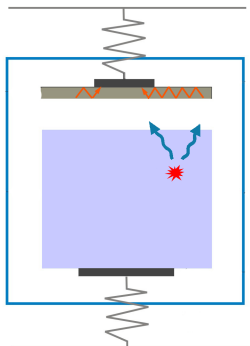
$$\rho \cdot E_{dep}$$

Energy Signal measured in the Light Channel



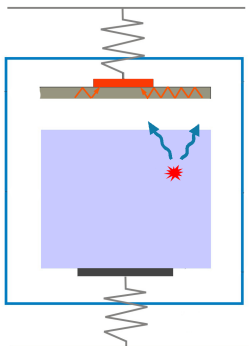
$$p \cdot q \cdot E_{dep}$$

Energy Signal measured in the Light Channel



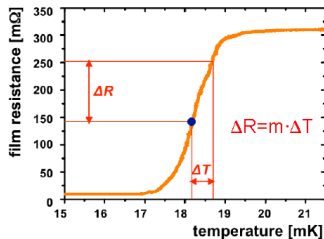
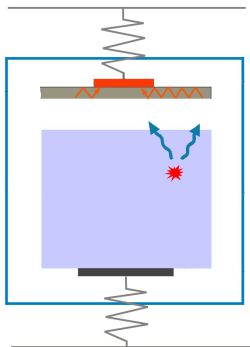
$$r \cdot p \cdot q \cdot E_{dep}$$

Energy Signal measured in the Light Channel



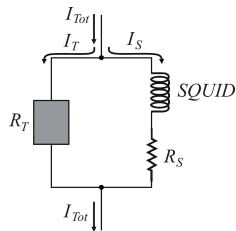
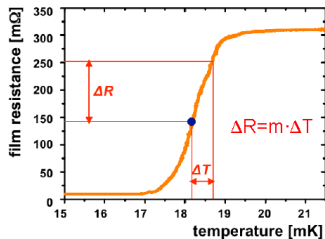
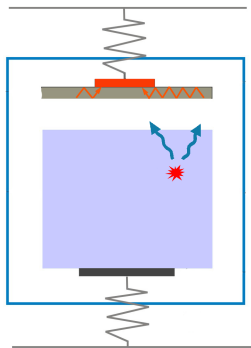
$$\frac{r}{C_T} \cdot p \cdot q \cdot E_{dep}$$

Energy Signal measured in the Light Channel



$$m \cdot \frac{r}{C_T} \cdot p \cdot q \cdot E_{dep}$$

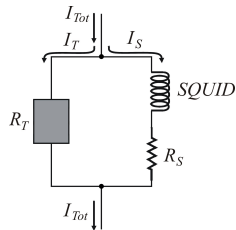
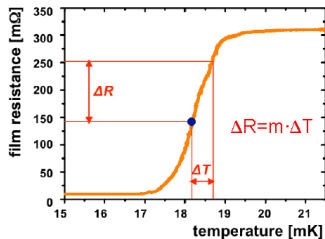
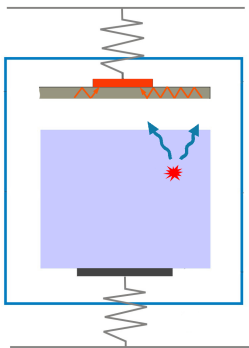
Energy Signal measured in the Light Channel



$$\Delta I_S = \frac{I_T}{R_S + R_T} \cdot \Delta R_T$$

$$\frac{I_T}{R_S + R_T} \cdot m \cdot \frac{r}{C_T} \cdot p \cdot q \cdot E_{dep}$$

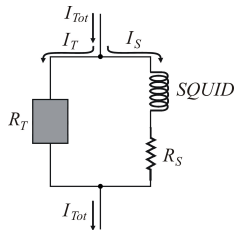
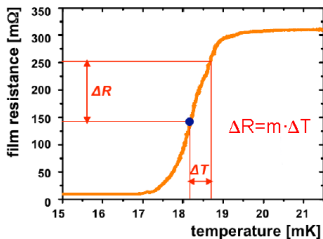
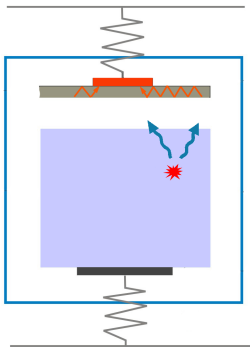
Energy Signal measured in the Light Channel



$$\Delta I_S = \frac{I_T}{R_S + R_T} \cdot \Delta R_T$$

$$\frac{\partial U}{\partial \Phi_0} \frac{\partial \Phi_0}{\partial I} \cdot \frac{I_T}{R_S + R_T} \cdot m \cdot \frac{r}{C_T} \cdot p \cdot q \cdot E_{dep}$$

Energy Signal measured in the Light Channel



$$\Delta I_S = \frac{I_T}{R_S + R_T} \cdot \Delta R_T$$

$$E = c \cdot \frac{\partial U}{\partial \Phi_0} \frac{\partial \Phi_0}{\partial I} \cdot \frac{I_T}{R_S + R_T} \cdot m \cdot \frac{r}{C_T} \cdot p \cdot q \cdot E_{dep}$$

Light Channel's Signal-to-Noise Ratio

Measured Energy

$$E = c \cdot \frac{\partial U}{\partial \Phi_0} \frac{\partial \Phi_0}{\partial I} \cdot \frac{I_T}{R_S + R_T} \cdot m \cdot \frac{r}{C_T} \cdot pq \cdot E_{dep}$$

Noise (@ $E = 0$)

$$\Delta E = \sqrt{I_J^2 + I_{SQ}^2 + I_{1/f}^2} = \sqrt{\frac{4k_B(T_C R_T + T_S R_S)}{(R_T + R_S)^2} + c_{SQ}^2 + f^2 \left(\frac{R_T}{R_n} \right)}$$

Light Channel's Signal-to-Noise Ratio

Measured Energy

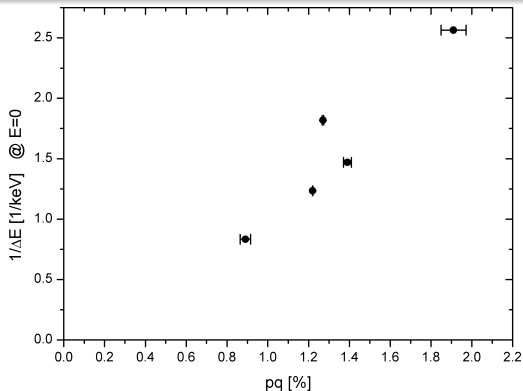
$$E = c \cdot \frac{\partial U}{\partial \Phi_0} \frac{\partial \Phi_0}{\partial I} \cdot \frac{I_T}{R_S + R_T} \cdot m \cdot \frac{r}{C_T} \cdot pq \cdot E_{dep}$$

Noise (@E = 0)

$$\Delta E = \sqrt{I_J^2 + I_{SQ}^2 + I_{1/f}^2} = \sqrt{\frac{4k_B(T_C R_T + T_S R_S)}{(R_T + R_S)^2} + C_{SQ}^2 + f^2 \left(\frac{R_T}{R_n} \right)}$$

Energy Fraction Absorbed by the Light Detector pq

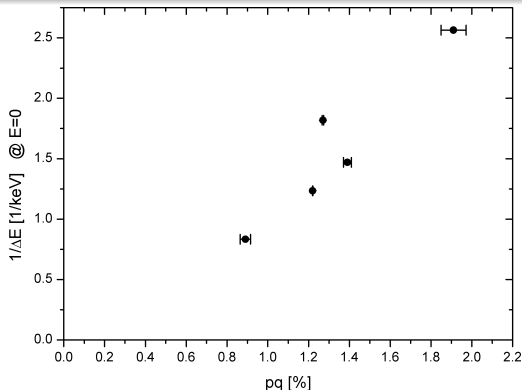
$$\frac{E}{\Delta E} \sim pq \text{ (@ } E = 0 \text{)}$$



Data of
CRESST
Light
Detectors

Energy Fraction Absorbed by the Light Detector pq

$$\frac{E}{\Delta E} \sim pq \text{ (@ } E = 0 \text{)}$$

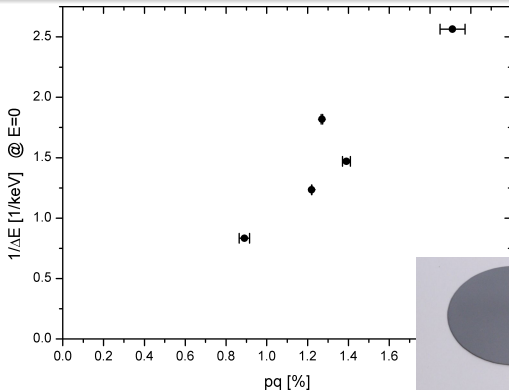


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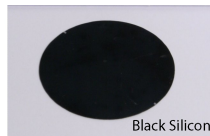
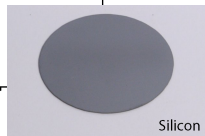
Increased sensitivity for improved light-production, -transport or -absorption

Energy Fraction Absorbed by the Light Detector pq

$$\frac{E}{\Delta E} \sim pq \quad (@E = 0)$$



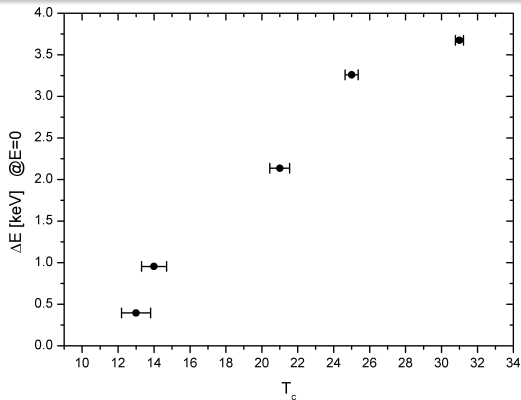
Data of
CRESST
Light
Detectors



Increased sensitivity for improved light-production, -transport or
-absorption → Black silicon

Transition Temperature T_C

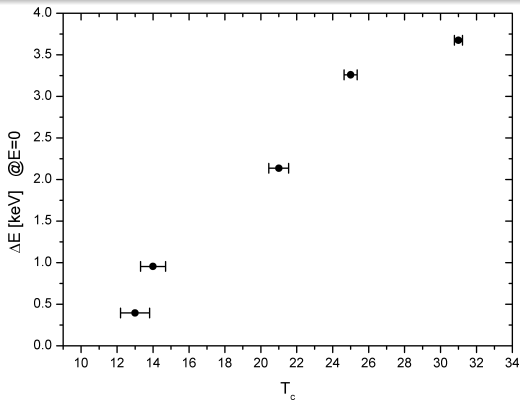
$$\frac{E}{\Delta E} \sim \frac{1}{C_T \cdot f(T_C)} \sim \frac{1}{T_C^{(1+\epsilon)}}$$



Data of
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Transition Temperature T_C

$$\frac{E}{\Delta E} \sim \frac{1}{C_T \cdot f(T_C)} \sim \frac{1}{T_C^{(1+\epsilon)}}$$

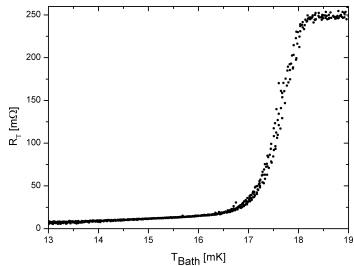


Data of
CRESST
Light
Detectors

Sensitivity improves for lower transition temperature

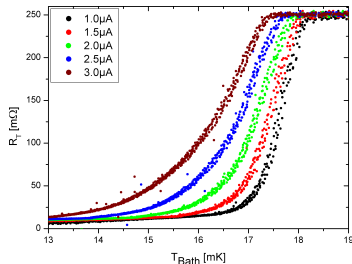
Transition Slope m

$$\frac{E}{\Delta E} \sim m = \frac{\Delta R}{\Delta T}$$



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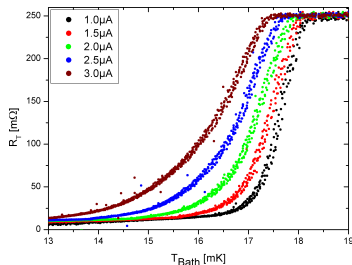


Transition slope m depends on read-out current

- Self-heating effect
- Critical current effect

Transition Slope m

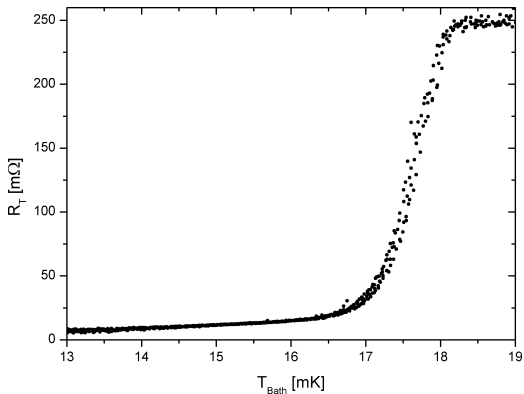
$$\frac{E}{\Delta E} \sim m = \frac{\Delta R}{\Delta T}$$



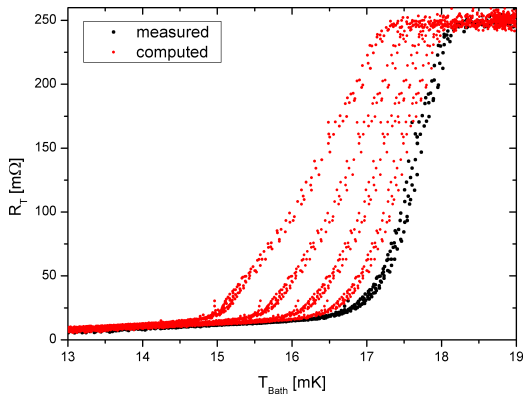
Transition slope m depends on read-out current

- Self-heating effect $\rightarrow \Delta T_{\text{Shift}} = \frac{P_T}{G_{BT}}$
- Critical current effect \rightarrow expected in the lower part of the transition

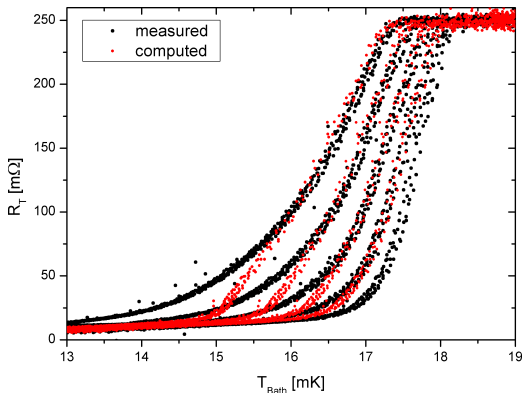
Calculation of the Self-Heating Effect



Calculation of the Self-Heating Effect

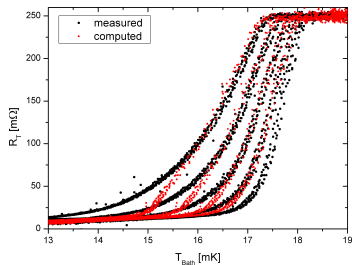


Calculation of the Self-Heating Effect

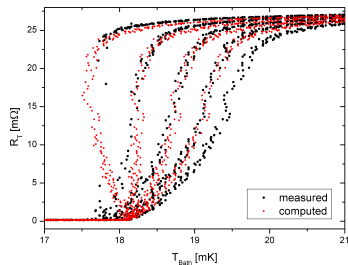


- Upper part of the transition can be explained with the self-heating effect
- Difference in the lower part of the transition due to the critical current effect

Reduction of the Normal Conducting Resistance R_n



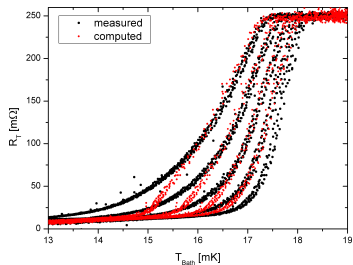
large R_n



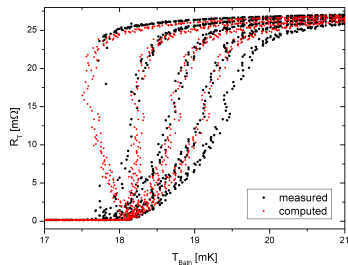
small R_n

Reduced critical current effect for small R_n

Reduction of the Normal Conducting Resistance R_n



large R_n



small R_n

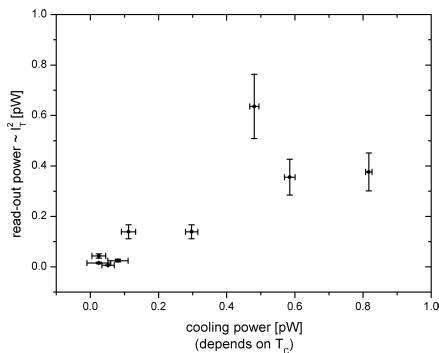
Reduced critical current effect for small R_n

small R_n opens the possibility for large transition slopes

Thermometer Current I_T

$$\frac{E}{\Delta E} \sim I_T$$

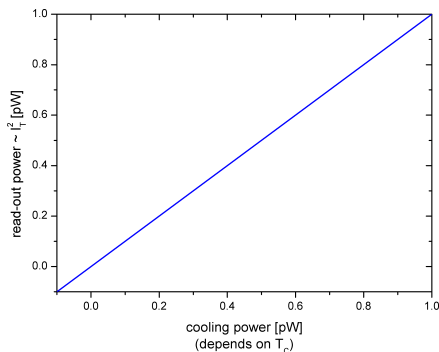
- Each light detector is optimized for best signal-to-noise $\rightarrow I_T$ fixed
- Limiting factors of thermometer current?



Thermometer Current I_T

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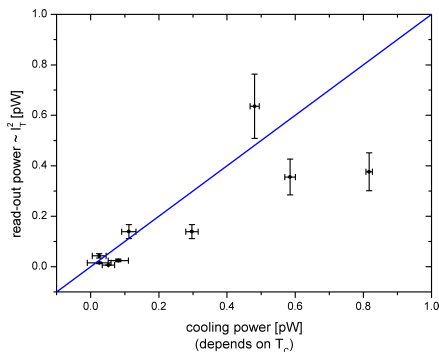
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Thermometer Current I_T

$$\frac{E}{\Delta E} \sim I_T$$

- Each light detector is optimized for best signal-to-noise $\rightarrow I_T$ fixed
- Limiting factors of thermometer current?



Thermometer current is mostly limited by cooling power

Thermal Coupling between Bath and Thermometer G_{BT}

- Increase of thermometer current I_T requires increase of cooling power
$$P_{BT} = G_{BT}(T_C - T_B)$$
- Transition temperature T_C and bath temperature T_B fixed
- Only thermal coupling G_{BT} can be adjusted

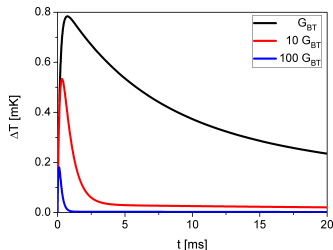
→ Increase of thermal coupling

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→ Increase of thermal coupling

- Temperature rise for given energy deposition reduced with larger thermal coupling



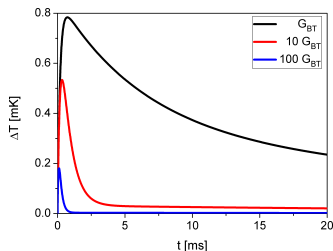
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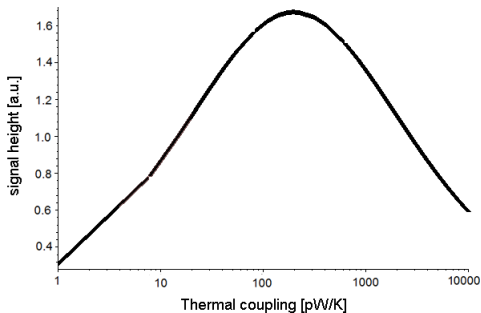
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→ Reduction of thermal coupling

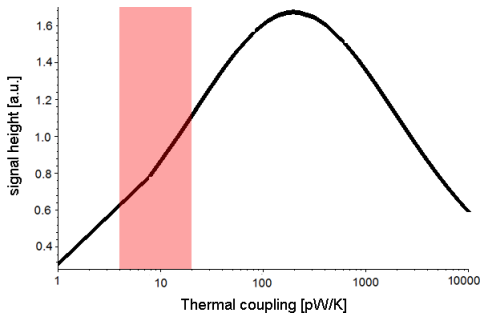
→ Optimization of thermal coupling

Signal height calculated for different thermal couplings



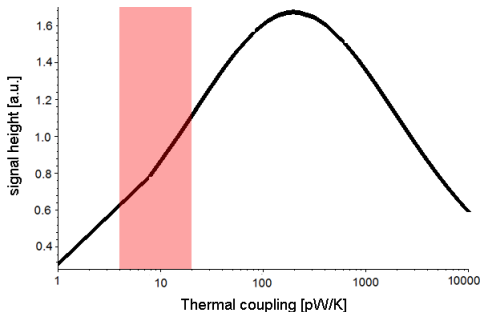
Optimization of the Thermal Coupling G_{BT}

Signal height calculated for different thermal couplings



Optimization of the Thermal Coupling G_{BT}

Signal height calculated for different thermal couplings



Largest signal expected for about ten times larger coupling

Motivation

Light channel energy resolution is the crucial factor for CRESST

Results

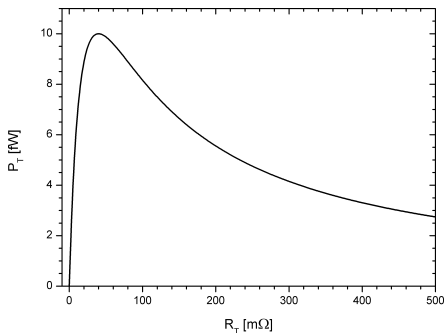
- Increase of light-production, -transport or -absorption
→ Black Silicon
- Lower transition temperature
→ Transition temperature of about 15 mK
- Larger transition slope
→ Reduction of critical current effect with smaller normal-conducting resistance
- Increased read-out current with optimized thermal coupling

Thank you for your attention

Backup

Self-Heating Effect

$$P_T = R_T I_T^2 = R_T I_{Tot}^2 \frac{R_S^2}{(R_S + R_T)^2}$$

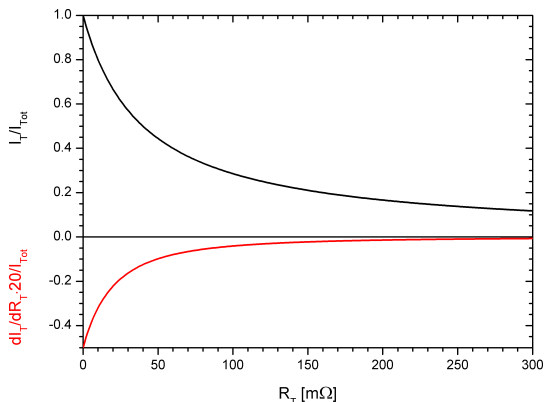


cooling power: $P_{BT} = (T_T - T_B)G_{BT}$

→ measured $\Delta T_{Shift} = T_T - T_B = \frac{P_T}{G_{BT}}$

Critical Current Effect

the thermometer current I_T influences the measured resistance



the change of the current dI_T influences the observed transition
→ critical current effect is expected to appear for $R_T \lesssim R_S$

Temperature Rise in the Thermometer

$$\Delta T_T = A_+ \left(e^{-\frac{t}{\tau_+}} - e^{-\frac{t}{\tau_N}} \right) + A_- \left(e^{-\frac{t}{\tau_-}} - e^{-\frac{t}{\tau_N}} \right) \quad (1)$$

$$= A_+(t) + A_-(t) \quad (2)$$

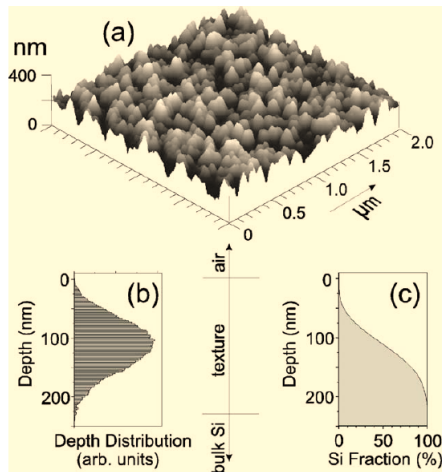
$$A_{\pm} = \frac{1}{1 - \frac{\tau_N}{\tau_{\pm}}} \cdot \frac{1}{\frac{1}{\tau_{\mp}} - \frac{1}{\tau_{\pm}}} \cdot \left[\varepsilon \cdot \left(\frac{1}{\tau_{\mp}} - \frac{G_{AT} + G_{BT}}{C_T} \right) + (1 - \varepsilon) \cdot \frac{G_{AT}}{C_A} \right] \cdot \frac{E_{LD}}{C_T} \quad (3)$$

$$\tau_{\pm} = \frac{2}{a \pm \sqrt{a^2 - 4b}} \quad (4)$$

$$a = \frac{G_{AT} + G_{BT}}{C_T} + \frac{G_{AT} + G_{AB}}{C_A} \quad (5)$$

$$b = \frac{G_{AT}G_{BT} + G_{AT}G_{AB} + G_{BT}G_{AB}}{C_T C_A} \quad (6)$$

Black Silicon



Detector Module

