Temperature and Strain Measurements With Optical Fibers in the Cryogenic Temperature Range

IMPRS EPP 13.11.2023

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Contents



- Why do we need a fiber optic measurement system?
- How it works
- Calibration
- First measurements
- Measurement of a high temperature superconducting coil
- Summary and outlook





AMS-100

Design requirements

- Geometric acceptance of $100 \text{ m}^2 \text{ sr}$ $\rightarrow 1000 \text{ times the acceptance of AMS-02}$
- Max. detectable rigidity of 100 TV
- Measurement of cosmic nuclei with energies up to the cosmic-ray knee

Planned design

- 3mm high temperature superconducting solenoid \rightarrow 0.5 T in a Volume of 75 m³
- Compensation coil
- Sun Shield
- Electric propulsion
- Radiator
- SciFi tracker
- Silicon tracker
- Time of flight system
- Calorimetry



High Temperature Superconducting Tape





Sensors



Limited weight budget

• Platinum resistors or strain gauges unsuitable as additional wiring is required for each sensor

Distributed temperature and strain monitoring with Rayleigh scattering and optical fibers



Fiber	Doping	$\operatorname{Core}/\operatorname{Cladding}/\operatorname{Coating} \varnothing \left[\mu m \right]$	Coating material
${ m SM1500}(9/125){ m P}$	Germanium	9/125/157	Polyimide
PS1250/1500	Boron	9/125/145	Acrylate

Optical Frequency Domain Reflectometry (OFDR)

RWTHAACHEN UNIVERSITY

- Light in an optical fiber can scatter at spectral index changes due to inhomogeneities ("Rayleigh Scattering")
- Each segment of an optical fiber has an individual Rayleigh scattering spectrum
- OFDR compares the changes between spectra for the same unloaded and loaded fiber segment

$$-\frac{\Delta\nu}{\hat{\nu}} = K_T \cdot \Delta T + K_\epsilon \cdot \epsilon$$
$$\Delta T = T_M - T_R \qquad \epsilon = \frac{\Delta L}{L}$$

OBR-4613, Luna Innovations



Girmen and Dittmar et al. 2023 [4] 7 Luna Innovations Inc. [5]

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Girmen and Dittmar et al. 2023 [4] ₈ Luna Innovations Inc. [5]

Non-Linear Model





Non-Linear Model





Strain Sensitivity

LN2



Test-Setup and conditions: Tensile test at 300 K and 77 K 0.86 Germanium - Fiber Boron - Fiber Two fibers glued in one groove 0.84 Slope, Dwyer et al. 2004 0.82 Strain gauge 0.80 Pt1000 **Optical fiber** 0.78 لٽ 0.76 LN2 LN2 container 0.74 0.72 0.70 100 150 200 Al tensile specimen T [K] Clamp

Strain Sensitivity as a Function of Temperature

Results:

- Slope corresponds to the literature for FBGs •
- Strain sensitivity is temperature dependent

300

250

Temperature Sensitivity Germanium



Test-Setup and conditions

- Warm-up (77 290 K, 18h)
- Climate chamber, 6 steps (233 335 K)
- Mechanical part considered by determining the thermal expansion of Al-6060 with calibrated strain gauges and the determined strain sensitivity





Results

Germanium-doped fibers:

- Quadratic temperature dependence
- Signal also at 77K

Temperature Sensitivity Boron



Test-Setup and conditions

- Warm-up (77 290 K, 18h)
- Climate chamber, 6 steps (233 335 K)
- Mechanical part considered by determining the thermal expansion of Al-6060 with calibrated strain gauges and the determined strain sensitivity





Results

Boron-doped fibers:

• Not sensitive to temperature < 150 K

Temperature Sensitivity



Test-Setup and conditions

- Warm-up (77 290 K, 18h)
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- Mechanical part considered by determining the thermal expansion of Al-6060 with calibrated strain gauges and the determined strain sensitivity





Results

- Germanium-doped fibers: linear temperature sensitivity
- Expected temperature sensitivity at 55 K: 0.5E-6 [1/K]
- Boron-doped fibers: not sensitive to temperature < 150 K

Test of Calibration: Germanium-doped Fiber



Test-Setup and conditions:

- Ring shaped Aluminum body
- 5 cm high, 15 cm diameter
- Both fibers glued in one Aluminum groove
- Warm-up (77 300 K, 18 h)
- Climate chamber, 6 steps (233 353 K)
- Shape similar to AMS-100 test coils





Calibration Test Germanium Fiber

Results:

- Well described across the total temperature range (77 K 353 K)
- Consistent with literature parameterization

Test of Calibration: Boron-doped Fiber



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- Shape similar to AMS-100 test coils





Calibration Test Boron Fiber

Results:

- Systematic drift at low temperatures
- Deviation within the prediction range



Test-Setup and conditions:

- HTS-Coil with 2.5 windings
- 10 cm high, 12 cm diameter
- 2 windings fiber under HTS-Tape glued in Aluminum
- Peek tubes for guiding the fibers into the structure







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Results:

- Temperature profile with maximum of 0.7 K
 - \rightarrow Current flows through Aluminum structure
- Magnetic field measurements: current flow of 800 900 A through the Aluminum structure at 1200A applied current

HTS – Test Coil: Dynamic T. Measurement



Test-Setup and conditions:

- HTS-Coil with 2.5 windings
- 10 cm high, 12 cm diameter
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- Peek tubes for guiding the fibers into the structure





Results:

- Temperature curve follows the current curve
- Changing current flows can be measured

Decoupling of Thermal & Mechanical Load

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- Combining two different fibers into one measurement
- Signal difference is due to the temperature sensitivity difference
- Newton method for function inversion

Test-Setup and conditions:

- **Ring shaped Aluminum body**
- 5cm high, 15cm diameter
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- Warm-up measurement (77 300 K, 18 h)





Decoupling of Thermal & Mechanical Load



- Combining two different fibers into one measurement
- Signal difference is due to the temperature sensitivity difference
- Newton method for function inversion

Test-Setup and conditions:

- Ring shaped Aluminum body
- 5cm high, 15cm diameter
- Both fibers glued in one Aluminum groove
- Warm-up measurement (77 300 K, 18 h)







Result:

Temperature resolution: 2.6 K for 77 – 100 K





- Germanium-doped SM fibers are sensitive to temperature changes down to 77 K and probably down to 55 K.
- Local heat sources and temperature profiles can be measured, and the sensitivity is highly dependent on the substrate.
- Decoupling with two differently doped fibers is possible, allowing temperature measurement with 2.6 K uncertainty.
- Published paper:

Girmen and Dittmar, 2023, "Young's modulus independent determination of fibre-parameters for Rayleigh-based optical frequency domain reflectometry from cryogenic temperatures up to 353K"

• Paper in preparation:

"New Measurement Principle for Decoupling Mechanical and Thermal Signals in OFDR Measurements for integrated Fibres"





Thank you for listening!

Are there any questions?

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HTS – Test Coil: Measurement 2



Test-Setup and conditions:

- HTS-Coil with 2.5 windings
- 10 cm high, 12 cm diameter
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• 3 additional Pt1000 and Kapton tape



HTS – Test Coil: Measurement 2



Test-Setup and conditions:

- HTS-Coil with 2.5 windings
- 10 cm high, 12 cm diameter
- 2 windings fiber under HTS-Tape glued in Aluminum
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• 3 additional Pt1000 and Kapton tape



Results:

- Temperature profile with maximum of 0.8 K
 - Mean temperature higher as without Pt1000
- Pt1000 position detectable

AMS-02

- The only operating particle detector with a magnet in space
 - measure charge, mass and velocity of charged particles
 - *Rigidity (momentum per unit charge)*
 - Can therefore distinguish particles from antiparticles
 - Measures precisely cosmic ray fluxes with an accuracy of 2%-4% at 100 GV

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Installed on the ISS since 2011

The Alpha Magnetic Spectrometer

Ex.: Positron Flux – Search for Dark Matter



Diffuse term: Low-energy part of the flux dominated by the positrons produced in the collisions of ordinary cosmic rays with the interstellar gas

Source term:

Origin through pulsars or dark matter anihilation or an unknown source

High Temperature Superconducting Coil



Coil Parameters

- Length of 6 m
- Diameter of 4 m
- Operating at 55 K
- Current 10 kA
- Layers of 12 mm HTS
- <u>Non-Isolated</u>
- <u>Aluminium U-Profile</u>

Highly protected against damage caused by quenching



HTS-Coil: Quench





32 Schael et al. (2022)[1]

HTS-Coil: Quench

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0





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Time after start of heating [min]



Description:

Loss of superconductivity over the entire coil with conversion of the stored magnetic field energy into heat

Reasons:

Local or global heating:

- External source
 - Cooling failure, heat input due to damaged detectors or damaged sun shield
- Current passing through the aluminum structure
 - Due to an internal local failure of the superconductivity by e.g. mechanical damage

Process:

- High heat input or extensive damage to the superconductor
 - Quench within a few seconds
- Low heat input which is greater than the cooling can remove
 - If local, current can bypasses non-superconducting region through aluminium structure
 - Coil can remain stable
 - When the current skips a whole turn, the effective number of turns carrying current changes, which induces current and heat throughout the coil, causing the coil to quench.

Temperature Sensitivity



Test-Setup and conditions

- Warm-up (77 290 K, 18h)
- Climate chamber, 6 steps (233 353 K)
- Mechanical part considered by determining the thermal expansion of Al-6060 with calibrated strain gauges and the determined strain sensitivity







Strain Sensitivity



Test-Setup and conditions:

- Tensile test at 300 K and 77 K
- Two fibers glued in one groove







LN2 LN2 container

Al tensile specimen



Strain Sensitivity



Test-Setup and conditions:

- Tensile test at 300 K and 77 K
- Two fibers glued in one groove





Tensile Test Germanium Fiber Data $Fit(x) = a + b \cdot x$ $a = 6.20e + 00 \pm 4.9e - 01$ 800 $b = 8.2899e-01 \pm 8.2e-04$ $\frac{\chi^2}{Ndf} = 0.1$ CI 0.95 600 Germanium Fiber -<u>∆</u>*E-6 + $T_{M} = 300 K$ 400 200 0 (Data - Fit(X))*E-6 20 \cap -20200 400 600 800 1000 0

Fiber	T [K]	$K_{\epsilon}(T)$
Germanium	300	$0.8290 \pm 0.8 \cdot 10^{-3} \text{ (stat) } \pm 5.0 \cdot 10^{-3} \text{ (sys)}$
Germanium	77	$0.7907 \pm 0.7 \cdot 10^{-3} \text{ (stat) } \pm 4.7 \cdot 10^{-3} \text{ (sys)}$
Boron	300	$0.8279 \pm 0.8 \cdot 10^{-3} \text{ (stat) } \pm 5.0 \cdot 10^{-3} \text{ (sys)}$
Boron	77	$0.7915 \pm 1.2 \cdot 10^{-3} \text{ (stat) } \pm 4.7 \cdot 10^{-3} \text{ (sys)}$

Strain*E-6

Tests with local thermal signals



Test-Setup and conditions:

• Heater on linear Aluminum and Peek structure in LN2



$$(T_M - T_R) = -\frac{\Delta\nu}{\hat{\nu}} \cdot \frac{1}{K_T(T_R) + K_\epsilon(T_R) \cdot CTE_{Substrate}}$$

Results:

- 1 cm external heating signals in LN2 can be measured
- Fiber temperature sensitivity depends on the CTE of the carrier material [CTE(PEEK) ≥ 2*CTE(AI)]





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Results:

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Strain Gauge Measurements









Resolution





	Germanium	Boron
Noise	0.8	0.6







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Magnetic Field Measurement





Magnetostriction

- Mechanical deformation in external magnetic field
- Dysprosium has a high mechanical deformation below 180K
- Epoxy dysprosium-powder mixture should have similar properties
- A bonded fiber should therefore be sensitive to magnetic fields at 77K
- 3 samples with nickel powder (test powder), dysprosium + nickel and dysprosium
- Measurement with and without homogeneous magnetic field
- Rotation in the magnetic field



Measurement in LN2





Freezer bag

Perdaix magnet Optical fiber





Pt1000 Temperature Sensor





Pt1000 Measured statistical nois

Back to the application





Conclusion:

Structure monitoring and quench protection is possible with the OFDR and multiple fibers.

Groove Width







OFDR Analysis



Rayleigh Backscatter Amplitude



Al-alloy skin for mechanical strength and axial thermal conductivity



Coil Model







Strain Sensitivity: Germanium doped fiber



RNTH

🖉 Fraunhofer

Strain Sensitivity: Boron doped fiber





Temperature Sensitivity: 233 K – 353 K





Reference Temperature check Germanium Fiber





Reference Temperature check Boron Fiber







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